



ISSN Print: 2394-7500  
 ISSN Online: 2394-5869  
 Impact Factor: 5.2  
 IJAR 2018; 4(1): 323-325  
 www.allresearchjournal.com  
 Received: 18-11-2017  
 Accepted: 23-12-2017

**Dr. Chandan Kumar**  
 Assistant Teacher, UHS  
 Belwa, Kashipur, Kishanganj,  
 Bihar, India

## Design the planar Sierpinski-gasket conical monopole antenna

**Dr. Chandan Kumar**

### Abstract

Planar Sierpinski monopole displays a multiband conduct, yet its boundaries in activity recurrence groups are not ideal. By planning the Sierpinski monopole on a cone like surface, a balanced three-dimensional (3-D) structure is gotten. Thusly, a bigger transmission capacity and a superior radiation design is accomplished. The even 3D Sierpinski-based monopole is a unique commitment of this paper. In the paper, various renditions of the funnel shaped Sierpinski based monopole are planned, and consequences of recreations acted in CST Microwave Studio are commonly thought about. At that point, the reenacted forms of the cone shaped monopole are advanced by determined standards. The enhanced funnel shaped Sierpinski-based monopole is fabricated and its properties are tentatively checked. Consequences of estimating the Sierpinski-based cone shaped monopole reception apparatus are distributed here unexpectedly. Sports. Besides this some psychological constraints stops some parents in showing the positive attitude.

**Keywords:** Sierpinski monopole, multi-band antenna, conformal antenna, fractals, conical monopole

### Introduction

In the present specialized gadgets, multi-band radio wires assume a pertinent job. The multi-band conduct of the radio wire can be gotten by putting forth a concentrated effort likenesses of fractals <sup>[1]</sup>. The quantity of activity recurrence groups relies upon the quantity of fractal cycles then <sup>[2]</sup>.

In this paper, methods of changing over a planar adaptation of the Sierpinski monopole to the conformal, funnel shaped radio wire are talked about. Following the portrayed way, two variants of the funnel shaped monopoles can be made. The planned receiving wires are displayed in CST Microwave Studio and their properties are commonly thought about. The primary sort of the funnel shaped monopole receiving wire was distributed in <sup>[3]</sup>, and the subsequent one is a unique commitment of this paper.

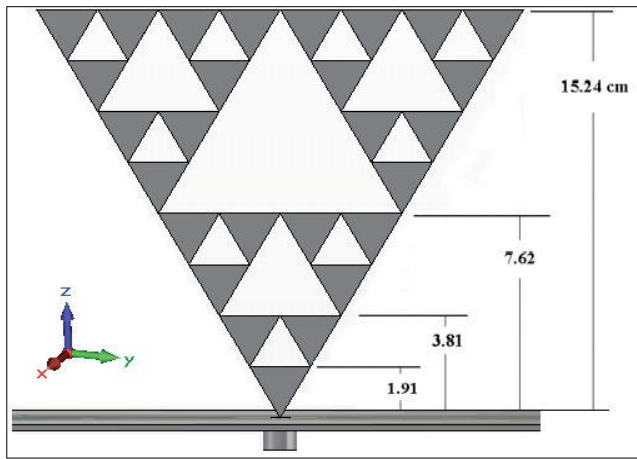
The planned tapered Sierpinski-based monopole is advanced utilizing molecule swarm streamlining (PSO) and the Nelder-Mead simplex calculation to arrive at an appropriate impedance coordinating in indicated recurrence groups. The advanced radio wire is estimated and results are contrasted and reproductions.

In Section 2, properties of a planar Sierpinski monopole and the changed gasket monopole radio wire are quickly investigated <sup>[4]</sup>. In Section 3, planar adaptations of radio wires are extended to the cone shaped surface <sup>[4]</sup>. Area 4 arrangements with the enhancement of planned receiving wires, and Section 5 presents trial results. Area 6 finishes up the paper.

### Planar Sierpinski Monopole

The planar Sierpinski monopole of the third order (Fig. 1) is created by 3 self-similar elements. The antenna is attached to the perfectly electrically conducting ground plane. At the antenna input, the SMA connector is assumed <sup>[4]</sup>.

**Correspondence**  
**Dr. Chandan Kumar**  
 Assistant Teacher, UHS  
 Belwa, Kashipur, Kishanganj,  
 Bihar, India

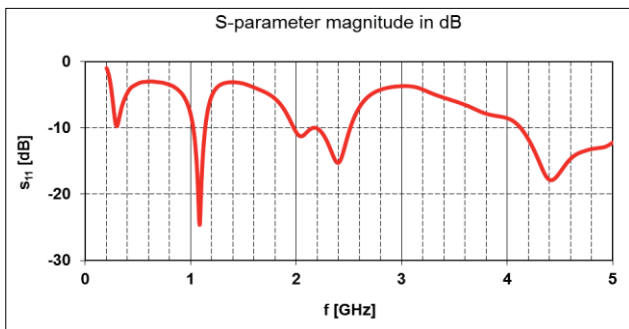


**Fig 1:** Sierpinski monopole.

In frequency response of the return loss (Fig. 2), the multi-band behavior can be observed (the first band reaches  $|S_{11}| = -9.74$  dB, the next three bands exhibiting  $|S_{11}| < -10$  dB for the reference impedance  $50 \Omega$ ) [4].

The lowest operation frequency is determined by the dimensions of the basic bowtie monopole. The higher operation frequencies are determined both by the basic bowtie structure and the triangular slots [4].

In the left-hand part of Tab. 1, magnitudes of  $S_{11}$  at the input of the planar Sierpinski monopole at the operation frequencies are summarized. Obviously,  $S_{11}$  does not reach the optimal values and bandwidths are narrow.



**Fig 2:** Frequency response of the planar Sierpinski monopole return loss.

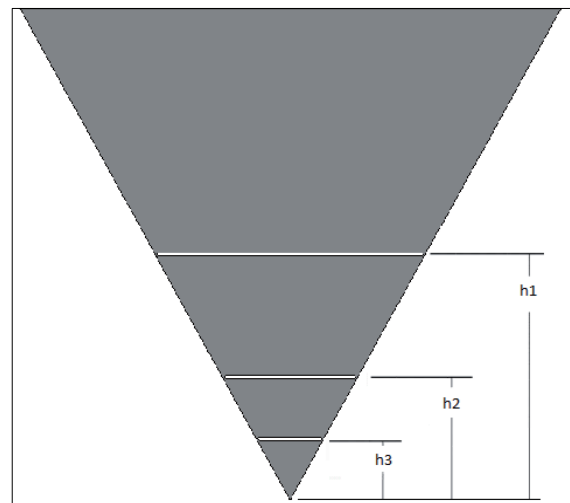
In order to improve the impedance matching, the concept of the modified gasket monopole antenna (Fig. 3) can be adopted [3]. The vertical distance of the slot from the ground plane equals to the height of the smallest triangles of the Sierpinski structure [4].

**Table 1:** Return loss of the conventional Sierpinski monopole (left) and the modified gasket monopole (right) at operation frequencies. Planar structure assumed.

Sierpinski monopole			Modified gasket monopole		
$f$ [GHz]	$S_{11}$ [dB]	BW [MHz]	$f$ [GHz]	$S_{11}$ [dB]	BW [MHz]
0.29	-9.74	71	0.31	-8.17	145
1.08	-24.63	25	1.18	-21.34	51
2.39	-15.28	180	2.66	-17.65	126
4.41	-17.89	243	4.63	-33.33	48

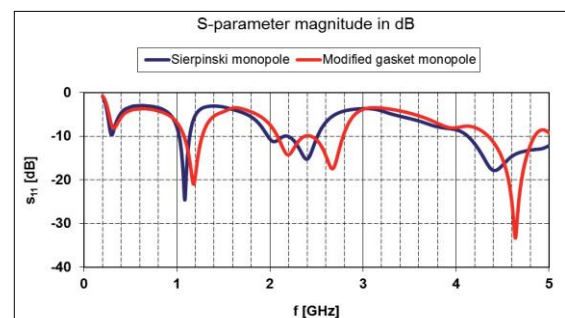
Frequency response of  $S_{11}$  of the modified gasket monopole is depicted in Fig. 4. In the right-hand part of Tab. 1,

magnitudes of  $S_{11}$  at operation frequencies are compared with the values of the Sierpinski monopole. The responses are similar.



**Fig 3:** Planar gasket monopole antenna.

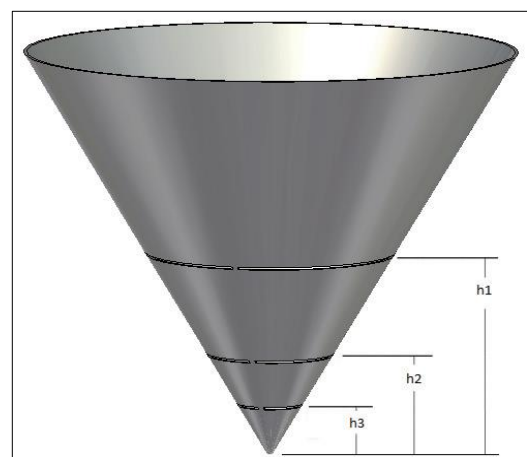
Radiation patterns of both planar antennas exhibit asymmetries caused by their asymmetrical geometry. In order to obtain the omni-directional pattern in the horizontal plane, geometries of planar antennas are projected into the conical surface [4].



**Fig 4:** Frequency response of return loss of the planar Sierpinski monopole (blue) and the gasket monopole antenna (red). Planar structures.

**Conical Sierpinski-Based Monopole**

In order to improve the symmetry of the radiation and to make the bandwidth wider, the planar structure is mapped [3] to the conical surface (Fig. 5).



**Fig 5:** Conical gasket monopole antenna.

Thanks to the conical shape, the omni-directional radiation and wider operation bandwidth are reached [3]. Heights of segments of the conical gasket monopole are identical with lengths of segments of the planar antenna.

Frequency response of the reflection coefficient at the antenna input  $S_{11}$  is depicted in Fig. 7. Magnitudes of the reflection coefficient in operation frequency bands are summarized in the right part of Tab. 2.

Next, the layout of the planar Sierpinski monopole was mapped to the conical surface (Fig. 6). The mapping resulted in an asymmetrical geometry. Heights of triangles of the conical antenna are identical with heights of triangles of the planar Sierpinski monopole.

The frequency response of the magnitude of the reflection coefficient  $S_{11}$  at the input of the conical Sierpinski-based monopole (Fig. 7) is similar to the characteristics of the planar Sierpinski monopole.

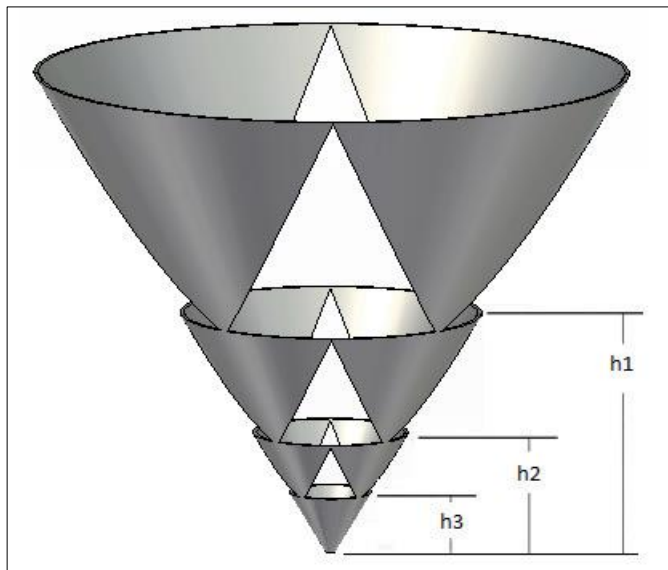


Fig 6: Conical Sierpinski-based monopole.

Values of  $S_{11}$  of the conical Sierpinski-based monopole in operation bands are given in the left-hand part of Tab. 2. Operation bands of the conical gasket monopole are shifted downwards, and the improvement of bandwidth with lower frequency is visible.

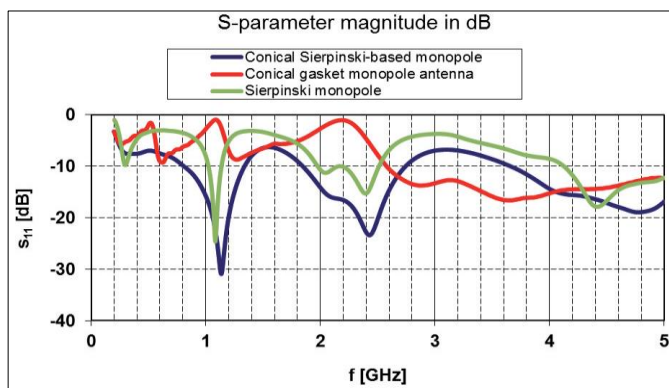


Fig 7: Frequency response of return loss of the conical Sierpinski-based monopole (blue) and the gasket one (red). Conical structures.

Radiation patterns of the conical gasket monopole are depicted. Here, the power improvement as well as the similarity of the radiation spectrum is obvious. The conical

Sierpinski-based monopole produces two beams, similar to a conventional monopole. Due to the symmetry of the structure in the vertical plane, an omnidirectional radiation character was achieved.

Table 2: Magnitude of  $S_{11}$  at the input of the conventional Sierpinski-based monopole (left) and the conical gasket monopole antenna (right) at operation frequencies. Conical structures assumed.

Conical Sierpinski-based monopole			Conical gasket monopole antenna		
$f$ [GHz]	$S_{11}$ [dB]	BW [MHz]	$f$ [GHz]	$S_{11}$ [dB]	BW [MHz]
0.38	-7.57..	-	0.24	-6.94..	-
1.13	-31.01..	76	0.60	-10.21..	231
2.42	-23.37..	16	1.25	-8.84..	368
4.74	-18.97..	476	2.87	-13.21..	-

Conclusions

Funnel shaped fractal reception apparatuses were gotten from the planar Sierpinski structure. By planning the planar design to the cone shaped surface, better omni-directional radiation and more extensive transmission capacity were reached.

The conelike gasket monopole shows the move of working groups and the impedance coordinating is more awful contrasted with the funnel shaped Sierpinski-based monopole. The data transmission of both the radio wires was expanded.

Radiation properties of both the cone shaped monopoles were improved. Additionally, resonances in comparative activity recurrence groups were reached.

Activity groups were tuned for the funnel shaped Sierpinski-based monopole, and the resultant radio wire was created. The deliberate outcomes somewhat vary from the reenactments.

The cone shaped Sierpinski-based monopole displays great impedance coordinating and great radiation properties. Then again, the size of this monopole is huge and the assembling is confounded.

References

1. Mandelbrot BB. The Fractal Geometry of Nature. New York: W.H. Freeman and Company, 1982.
2. Puente C, Romeu J, Pous R, Cardama A. On the behavior of the Sierpinski multiband fractal antenna. IEEE Transactions on Antennas and Propagation 1998;46(4):517-524.
3. Best SR. A multiband conical monopole antenna derived from a modified Sierpinski gasket. IEEE Antennas and Wireless Propagation Letters 2003;2:205-207.
4. Všetula P, Raida Z. Sierpinski conical monopole antennas. In Proceedings of the 15th Conference on Microwave Techniques COMITE. Brno (Czech Republic), 2010, p55-57.